

Wokshop on microflow calibration methods:

Optical Methods

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Abir Wissam Boudaoud, PhD Student, abir-wissam.boudaoud@cetiat.fr

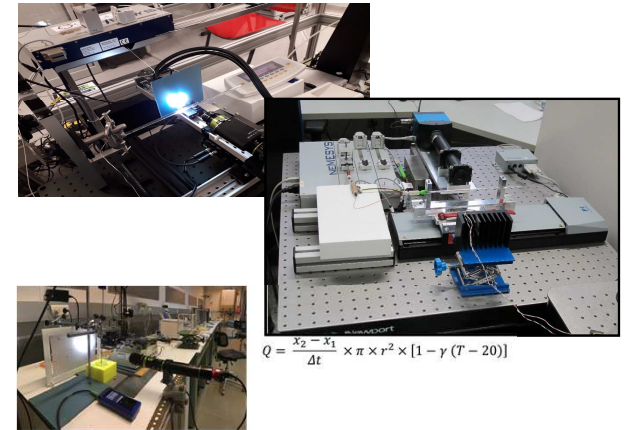


18th Nov. 2020

Overview

1. Interface tracking method

- Principle (example at CETIAT)
- Uncertainty budget (example at CETIAT)
- IPQ & THL Interface Tracking Setups

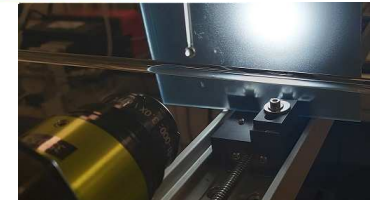


$$Q = \frac{x_2 - x_1}{\Delta t} \times \pi \times r^2 \times [1 - \gamma (T - 20)]$$

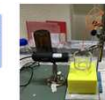
2. Pendant drop method

- Principle (example at CETIAT)
- IPQ Pendant Drop setup

Can go down 1 $\mu\text{L/h}$ with 7 % uncertainty



The delivered liquid flow was determined by observing the volume increase of a drop at the end of the flow line placed inside an evaporation trap.



This observation was performed at a specific time by using photographs taken by a digital USB microscope with 400X magnification and a Python software for image treatment.

$$Q = \frac{\Delta V}{\Delta t}$$

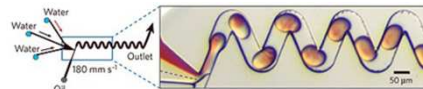
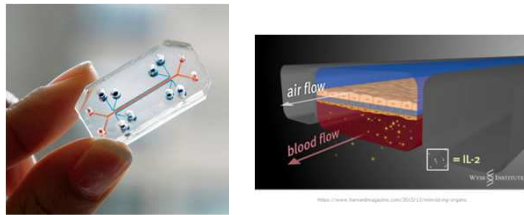
Optical nano-flow standards



- Micro-flow = **1 ml/h (16 μ l/min)** to 1 L/h (16 ml/min)
1 drop/ minute to 5 drop/ second
- Nano-flow = **\sim 1 μ l/h (16 nl/min)** to 1 ml/h (16 μ l/min)
1 drop/ month to 1 drop / minute



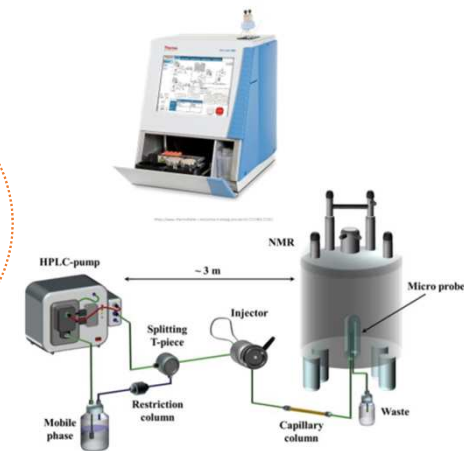
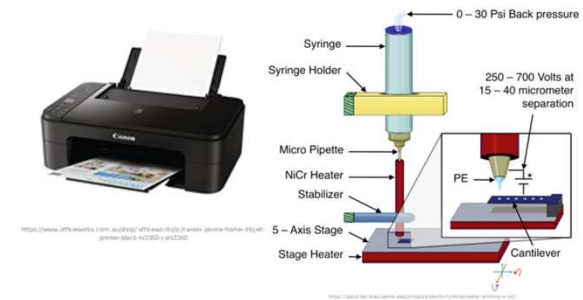
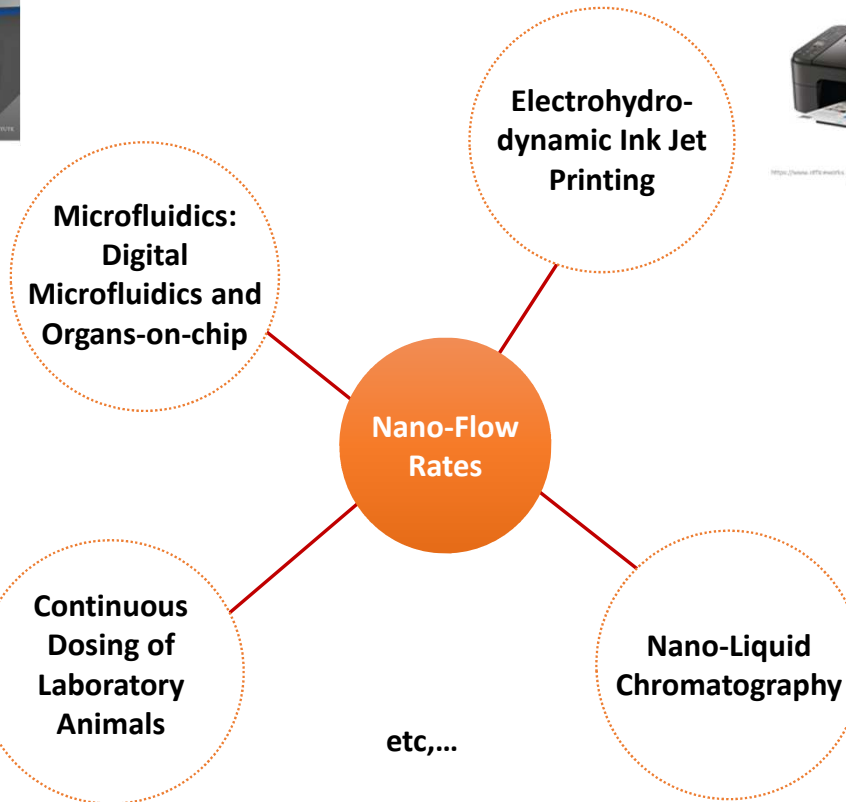
Optical nano-flow standards: applications



DeHells, Andrew. (2006). Control and detection of chemical reactions in microfluidic systems. Nature, 442, 394-402. 10.1038/nature05062.



<https://www.abax.com/>

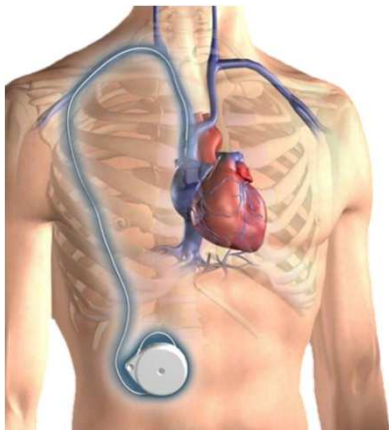


WILLIAMS, Gary, WILKINS, Jonathan, Theory and Practice of HPLC and UPLC/CE, in: HODGKIN, M. B., BURDICK, C. Handbook of Molecular Chromatography/Phase Separation Technology, ACS Press, 2011, p. 1-18.

Optical nano-flow standards: applications



Implantable Infusion Pumps



<https://docplayer.net/82396718-United-therapeutics-corporation.html>



<https://www.medtronic.com/us-en/healthcare-professionals/products/neurological/drug-infusion-systems/synchromed-ii.html>



<https://bmccancer.biomedcentral.com/articles/10.1186/s12885-019-5515-6/figures/2>

Flow rates range : 0,048 ml/day → 3 ml/day
 $Q_L \text{ min} = 33 \text{ nl/min}$

Insulin Pumps



<https://myglu.org/articles/sales-of-medtronic-paradigm-pump-line-discontinued>



<https://www.omnipod.com/fr-ch/educational-resources/videos>



<https://www.medtronic-diabetes.co.uk/insulin-pump-therapy/minimed-640g-system>

Basal rate: 0,02 U/h → 50 U/h
 $Q_L \text{ min} = 3 \text{ nl/min}$

Optical nano-flow standards: applications



Implantable Infusion Pumps



<https://docplayer.net/8239671>

Insulin Pumps



<https://www.medtronic-diabetes.co.uk/insulin-pump-therapy/minimed-640g-system>

Need to be calibrated against primary standards to ensure the traceability of measurements to the I.S. of Units!

Flow rates range : 0,048 ml/day → 3 ml/day
 $Q_{L \text{ min}} = 33 \text{ nl/min}$

Basal rate: 0,02 U/h → 50 U/h
 $Q_{L \text{ min}} = 3 \text{ nl/min}$

Optical nano-flow standards: MeDDII project



The EMPIR initiative is co-funded by the European Union's Horizon 2020 research and innovation programme and the EMPIR Participating States

→ To develop primary standards down to 5 nl/min with expanded uncertainty of 2% (k=2)



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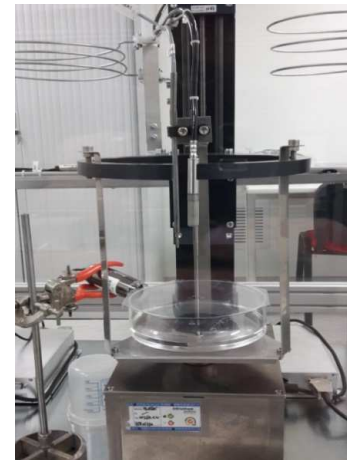
Microflow standards (MeDD I)



CETIAT's micro-flow bench



Gravimetric Method



$$Q = \frac{\Delta m}{\Delta t}$$

The laboratory of liquid flow and micro-liquid flow measurement is COFRAC accredited for flow rates going down to 16 μ L/min with best U(k=2) = 0.1%



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Optical nano-flow standards at CETIAT



- Ongoing PhD Thesis collaboration
- PhD student: **Abir Wissam Boudaoud**



Teresa LOPEZ-LEON and Joshua D. McGraw

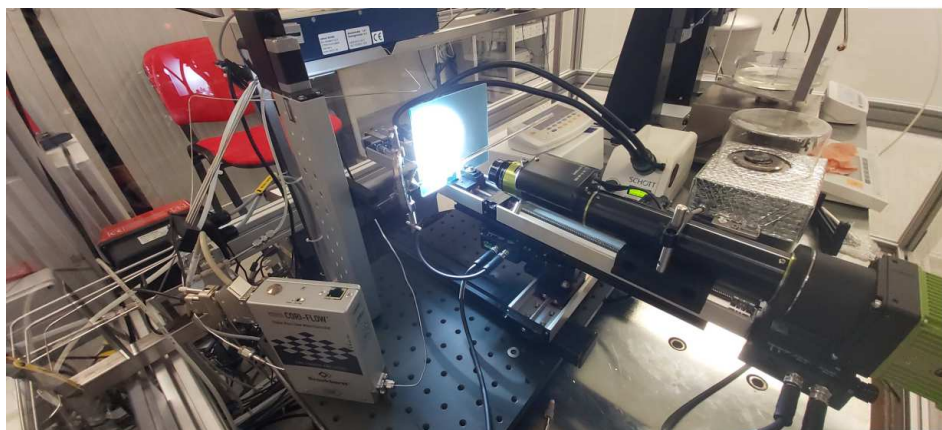
➔ Development of a primary standard for nano-flow rates of liquids

EMPIR

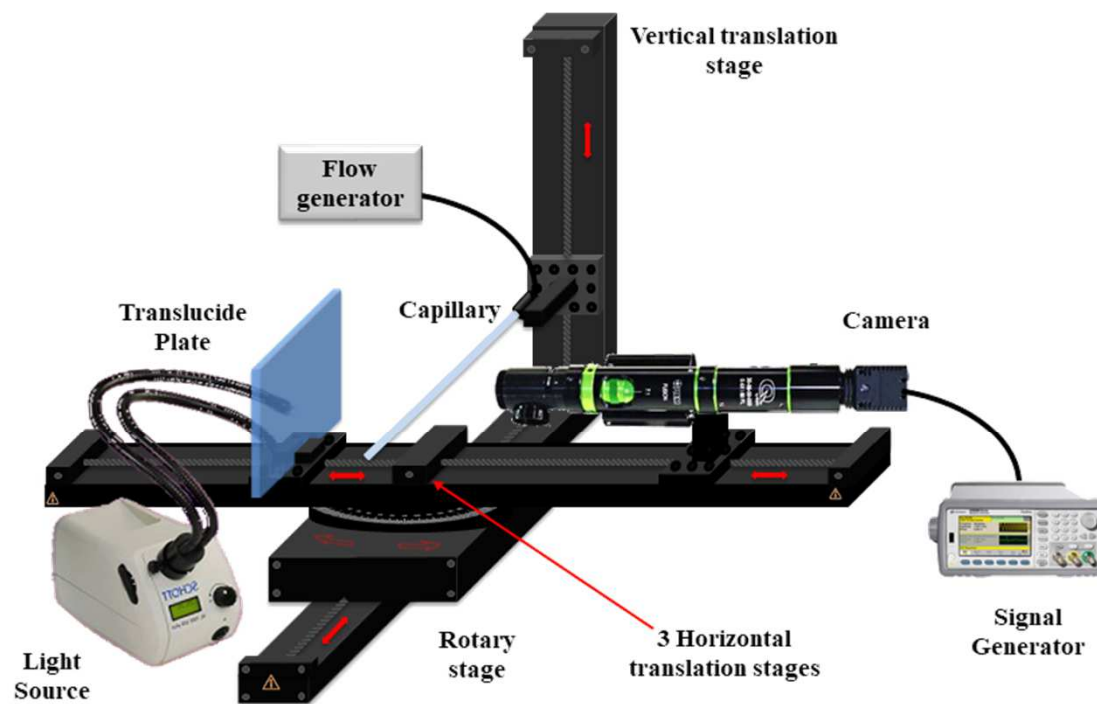


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Interface Tracking: principle at CETIAT

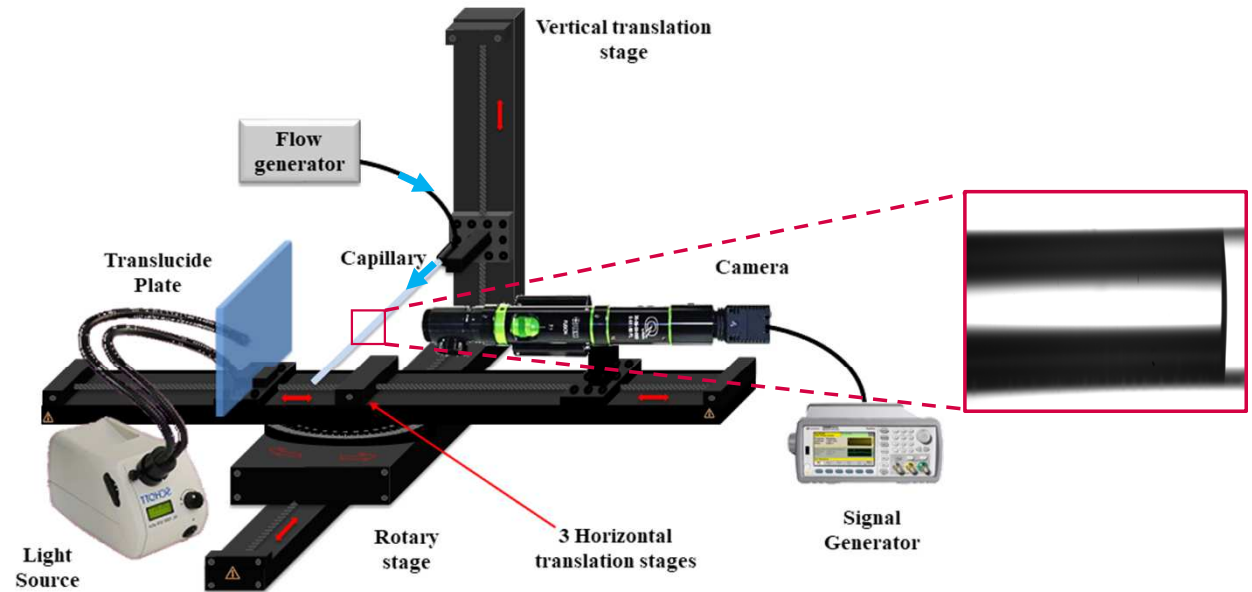


CETIAT's Interface Tracking calibration system

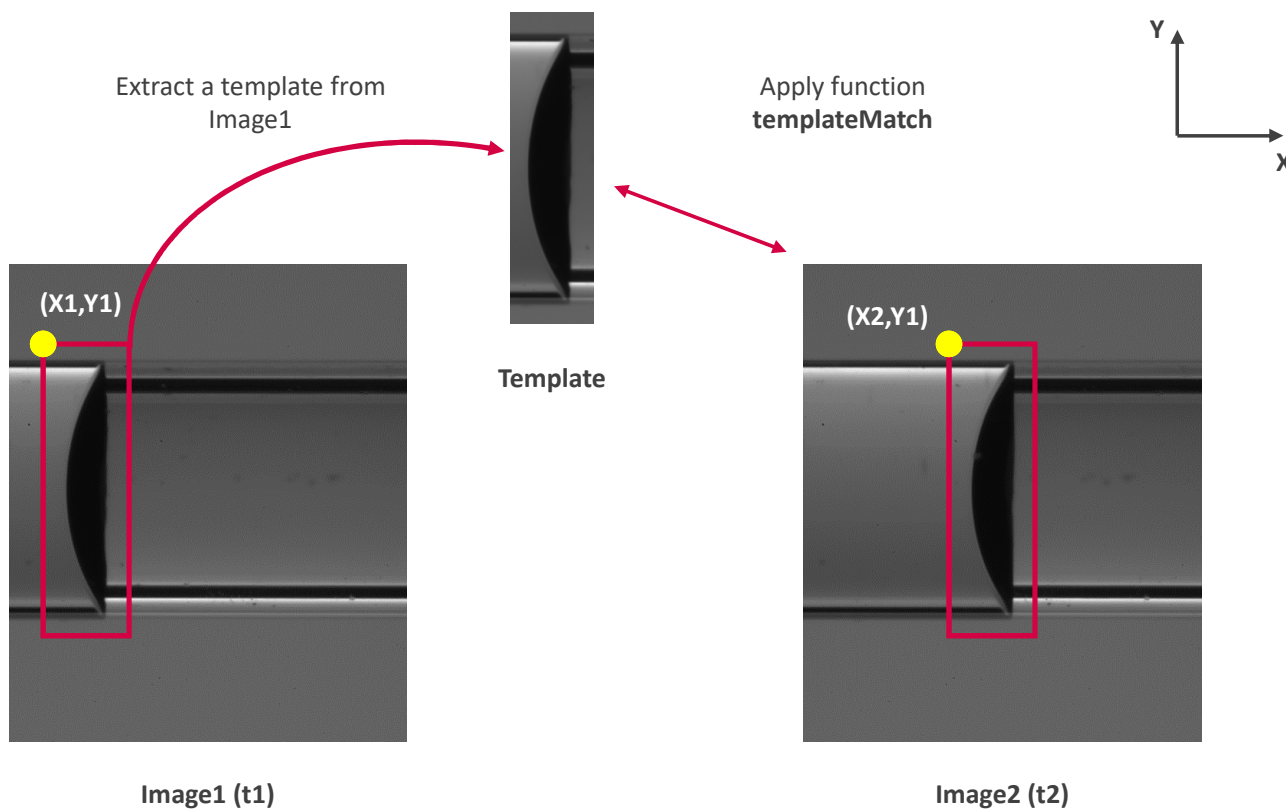


Interface Tracking: principle at CETIAT

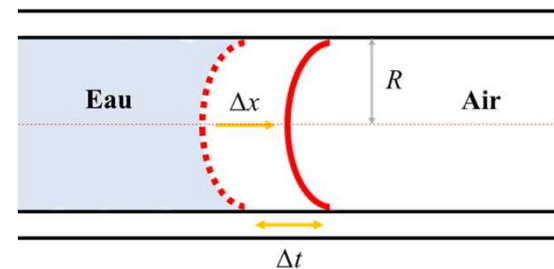
1. Generation of a liquid flow
2. Image acquisition of the liquid/air interface once this one enters in the camera's field of view
3. Measurement of the interface's displacement by image processing



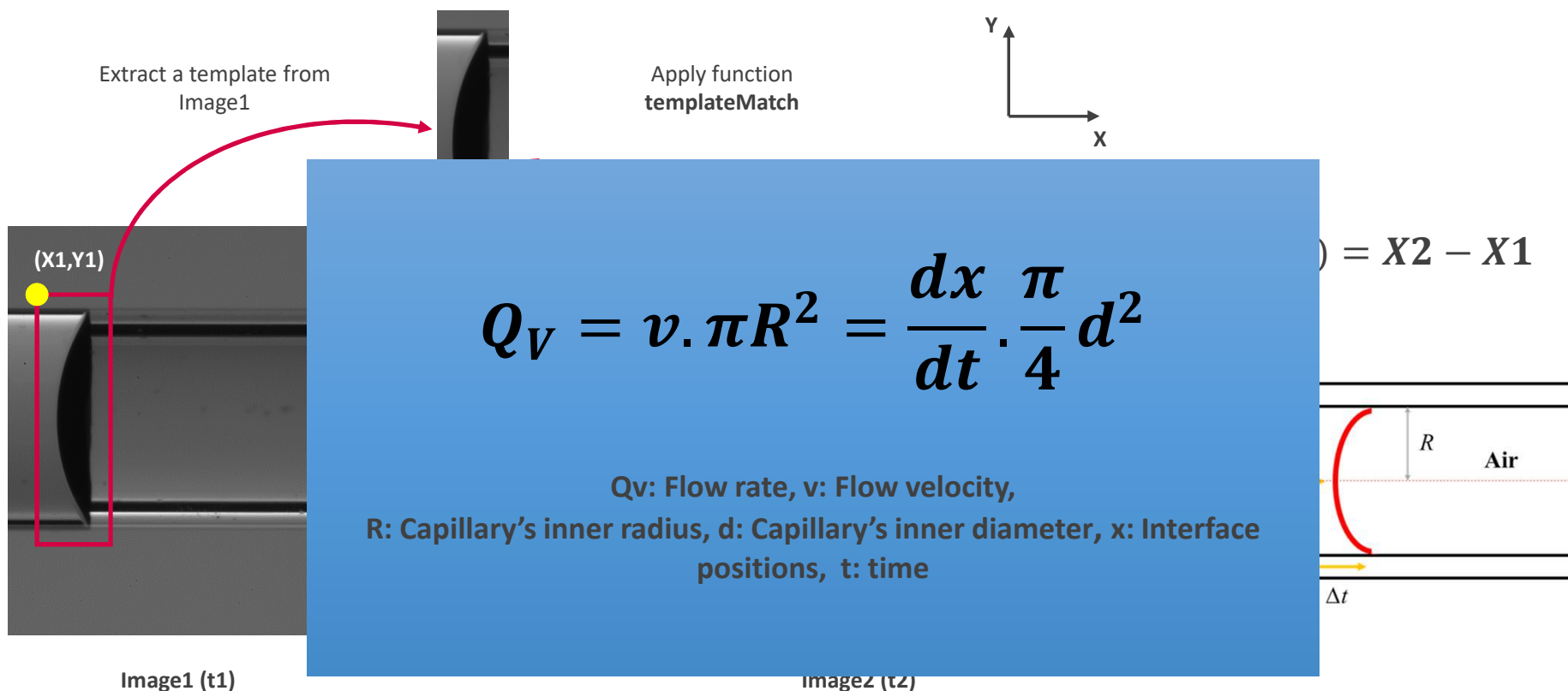
Interface Tracking: principle at CETIAT



$$\Delta X(t1, t2) = X2 - X1$$



Interface Tracking: principle at CETIAT

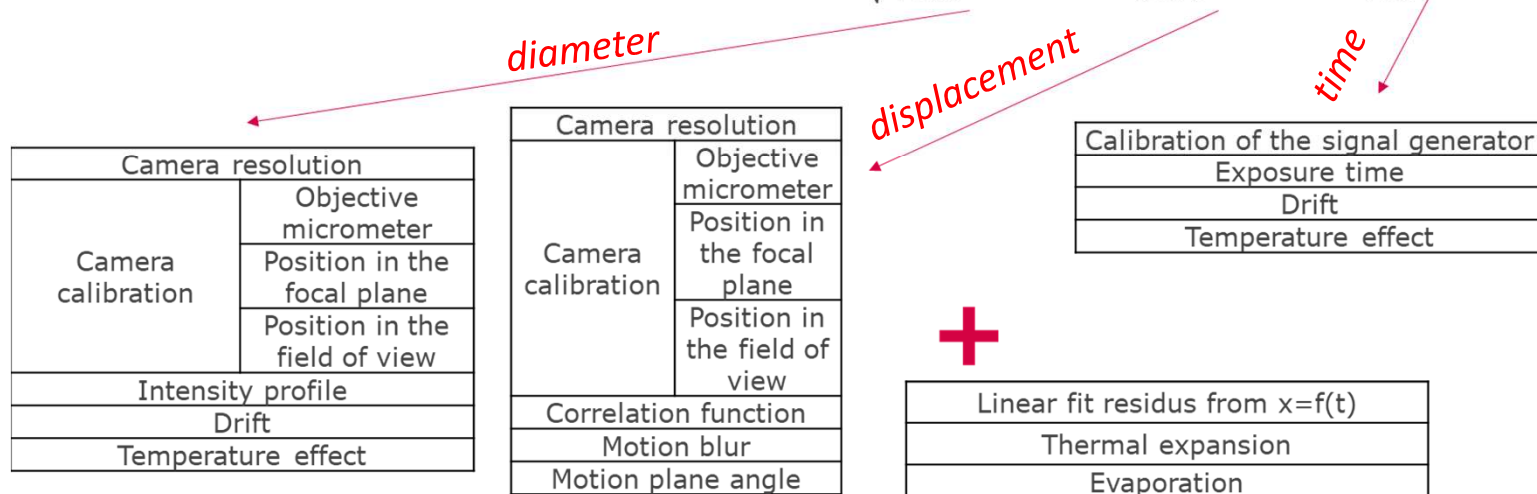


Interface Tracking: principle at CETIAT Uncertainty Budget



Flow rate : $Q_V = v \cdot \pi R^2 = \frac{x}{t} \cdot \frac{\pi}{4} R^2$

Measurement uncertainty : $u(Q_V) = \sqrt{\left(\frac{\partial Q_V}{\partial d}\right)^2 \cdot u^2(d) + \left(\frac{\partial Q_V}{\partial x}\right)^2 \cdot u^2(x) + \left(\frac{\partial Q_V}{\partial t}\right)^2 \cdot u^2(t)}$



For 5 nl/min :

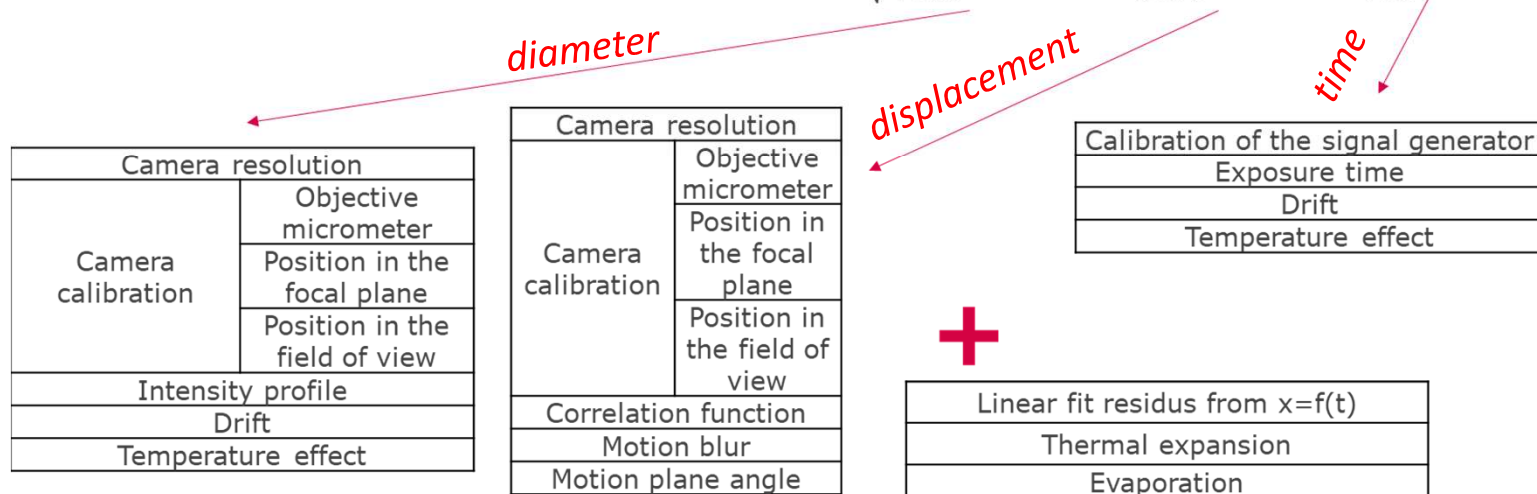
$U(Q_{ref}) = 11 \% (k=2)$ for a 1 second measurement at 5 fps

$U(Q_{ref}) = 0.5 \% (k=2)$ for a 120 seconds measurement at 5 fps

Interface Tracking: principle at CETIAT Uncertainty Budget

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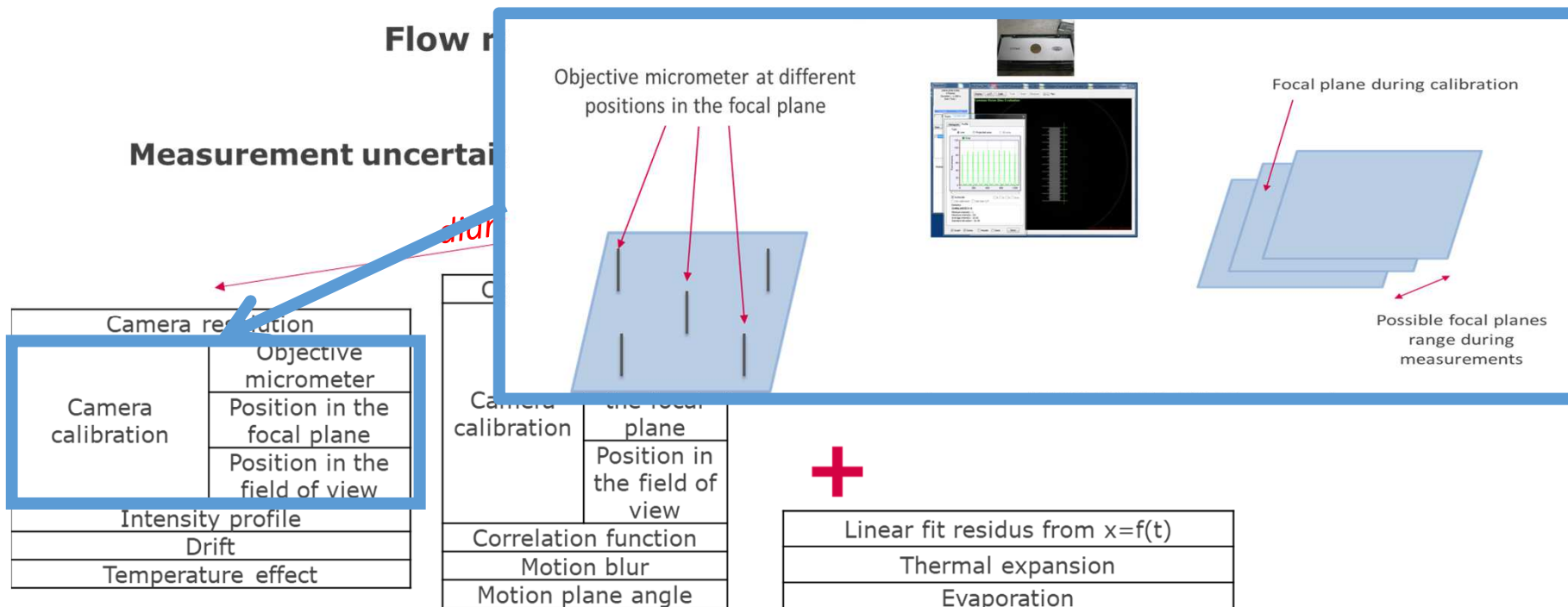


For 5 nl/min :

$U(Q_{ref}) = 11 \% (k=2)$ for a 1 second measurement at 5 fps

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Interface Tracking: principle at CETIAT Uncertainty Budget



For 5 nl/min :

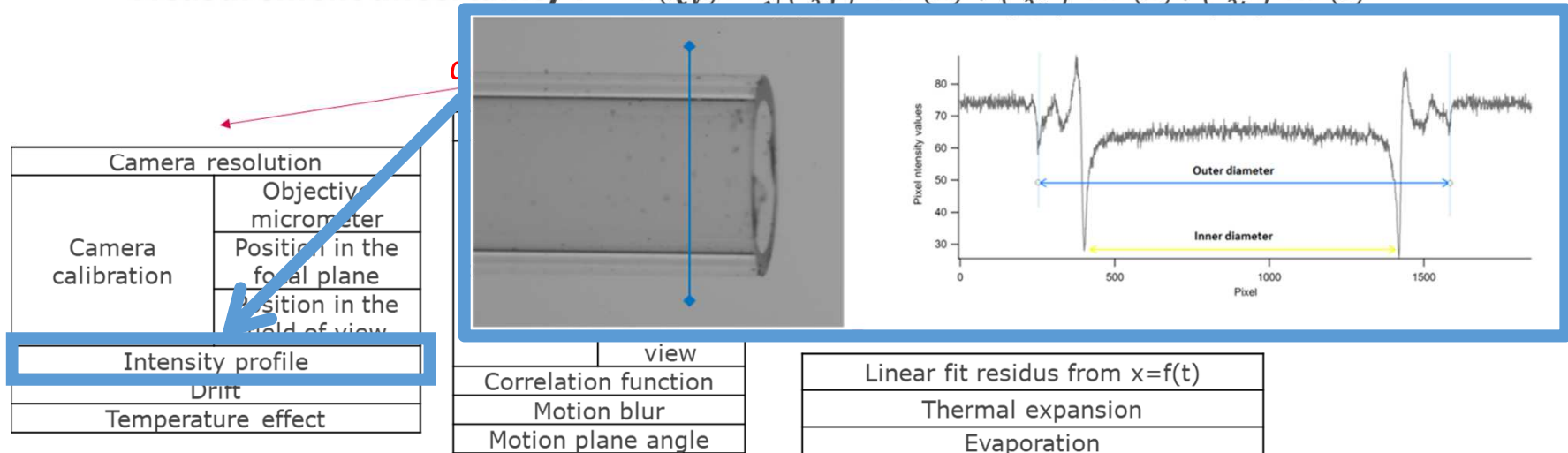
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For 5 nl/min :

$U(Q_{ref}) = 11 \% (k=2)$ for a 1 second measurement at 5 fps

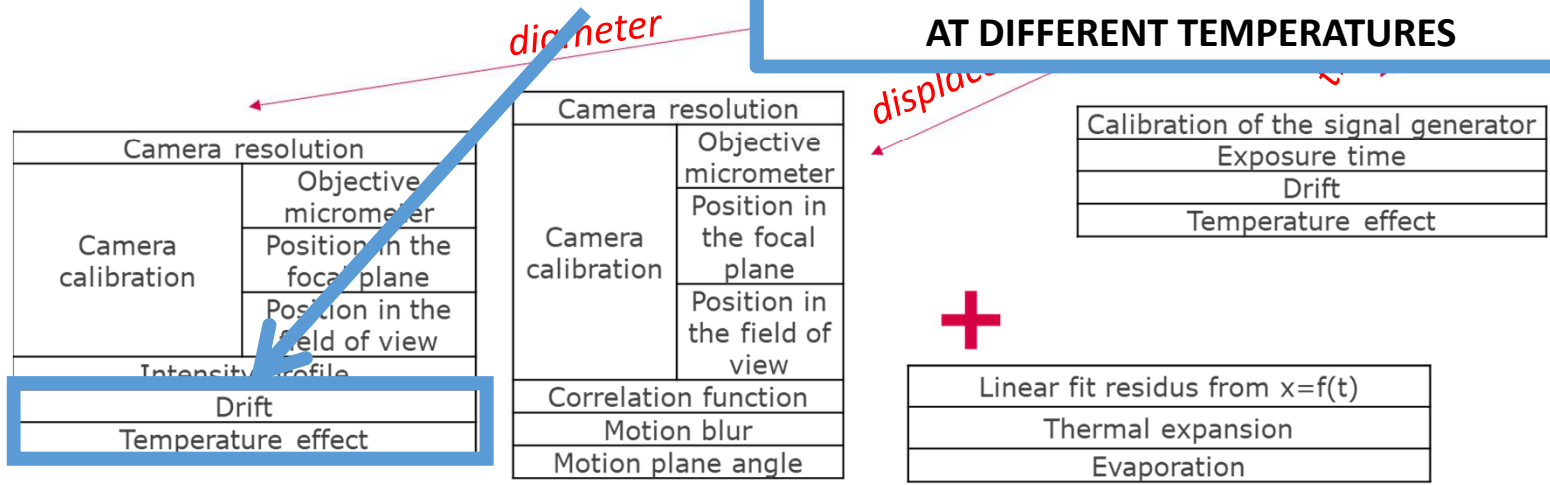
$U(Q_{ref}) = 0.5 \% (k=2)$ for a 120 seconds measurement at 5 fps

Interface Tracking: principle at CETIAT Uncertainty Budget



Flow rate : $Q_V = v \cdot \pi R^2 = \frac{x}{t} \cdot \frac{\pi}{4} R^2$

Measurement uncertainty : u **EVALUATED BY SUCCESSIVE CALIBRATIONS AND AT DIFFERENT TEMPERATURES**



For 5 nl/min :

$U(Q_{ref}) = 11 \% (k=2)$ for a 1 second measurement at 5 fps

$U(Q_{ref}) = 0.5 \% (k=2)$ for a 120 seconds measurement at 5 fps



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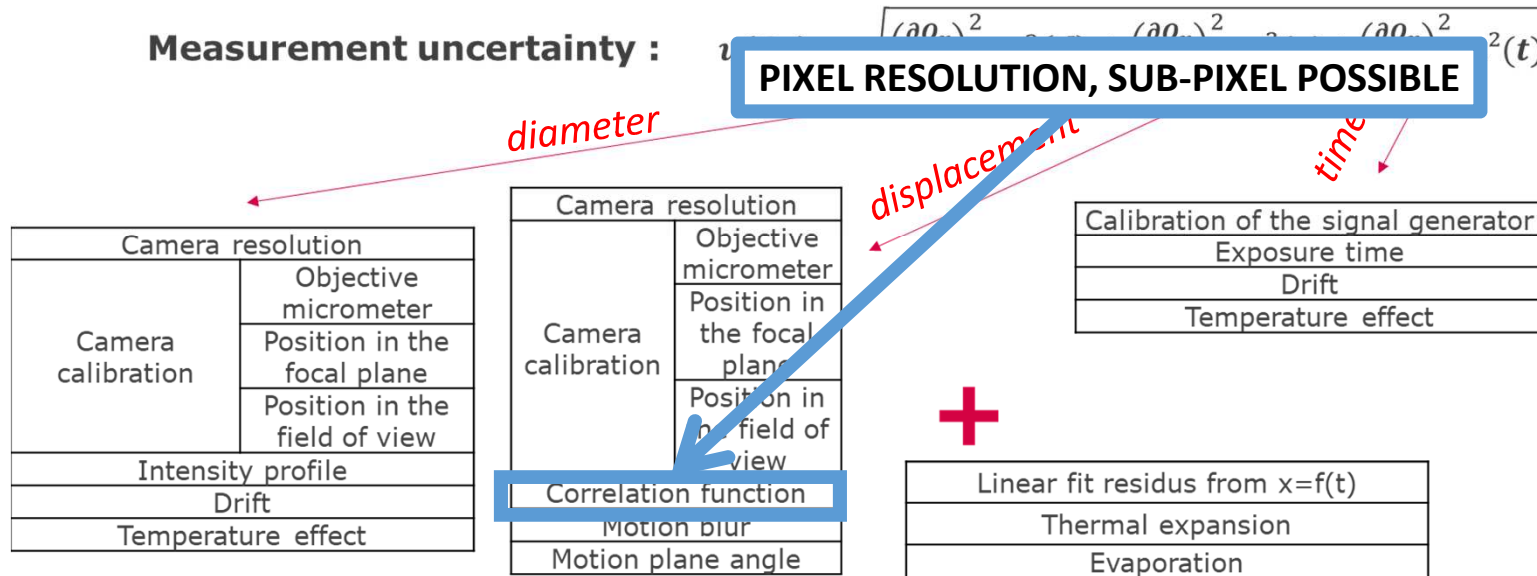
Interface Tracking: principle at CETIAT Uncertainty Budget



Flow rate : $Q_V = v \cdot \pi R^2 = \frac{x}{t} \cdot \frac{\pi}{4} R^2$

Measurement uncertainty :

PIXEL RESOLUTION, SUB-PIXEL POSSIBLE



For 5 nl/min :

$U(Q_{ref}) = 11 \% (k=2)$ for a 1 second measurement at 5 fps

$U(Q_{ref}) = 0.5 \% (k=2)$ for a 120 seconds measurement at 5 fps



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Interface Tracking: principle at CETIAT Uncertainty Budget



Flow rate : $Q_V = v \cdot \pi R^2 = \frac{x}{t} \cdot \frac{\pi}{4} R^2$

Measurement uncertainty : $u(Q_{ref})$

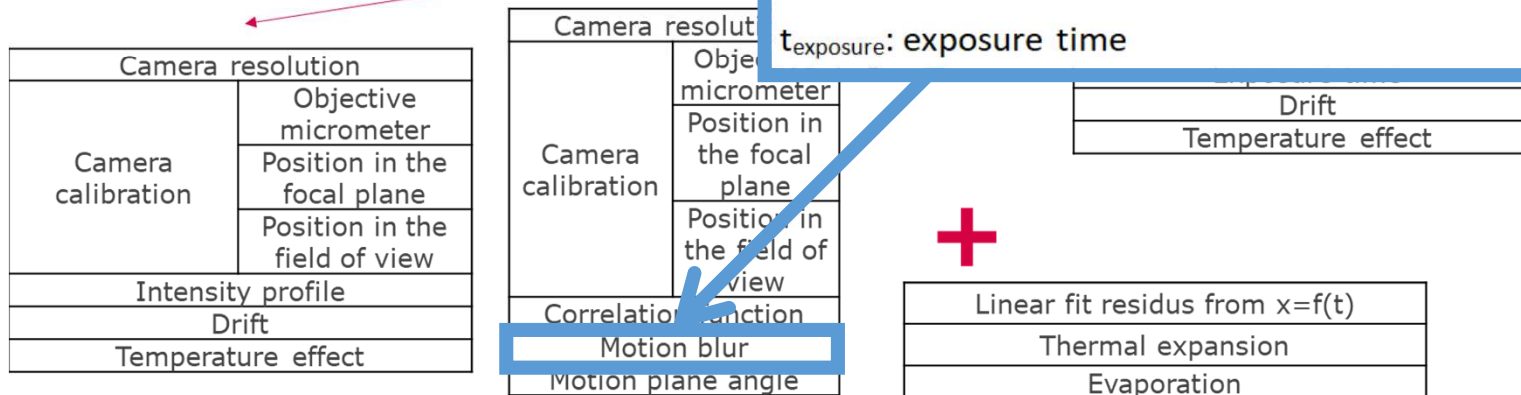
Distance D travelled by the interface during exposure time:

$$D = v \cdot t_{exposure}$$

V: Interface displacement velocity

$t_{exposure}$: exposure time

diameter



For 5 nl/min :

$U(Q_{ref}) = 11 \% (k=2)$ for a 1 second measurement at 5 fps

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Interface Tracking: principle at CETIAT Uncertainty Budget



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Measurement uncertainty : $u(Q_{ref})$

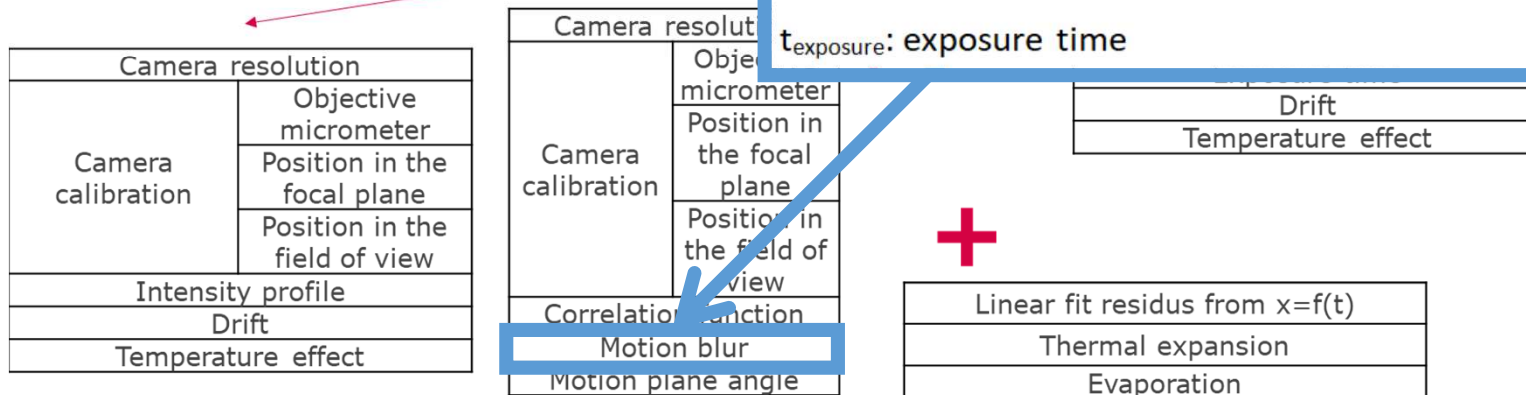
Distance D travelled by the interface during exposure time:

$$D = v \cdot t_{exposure}$$

V: Interface displacement velocity

$t_{exposure}$: exposure time

diameter

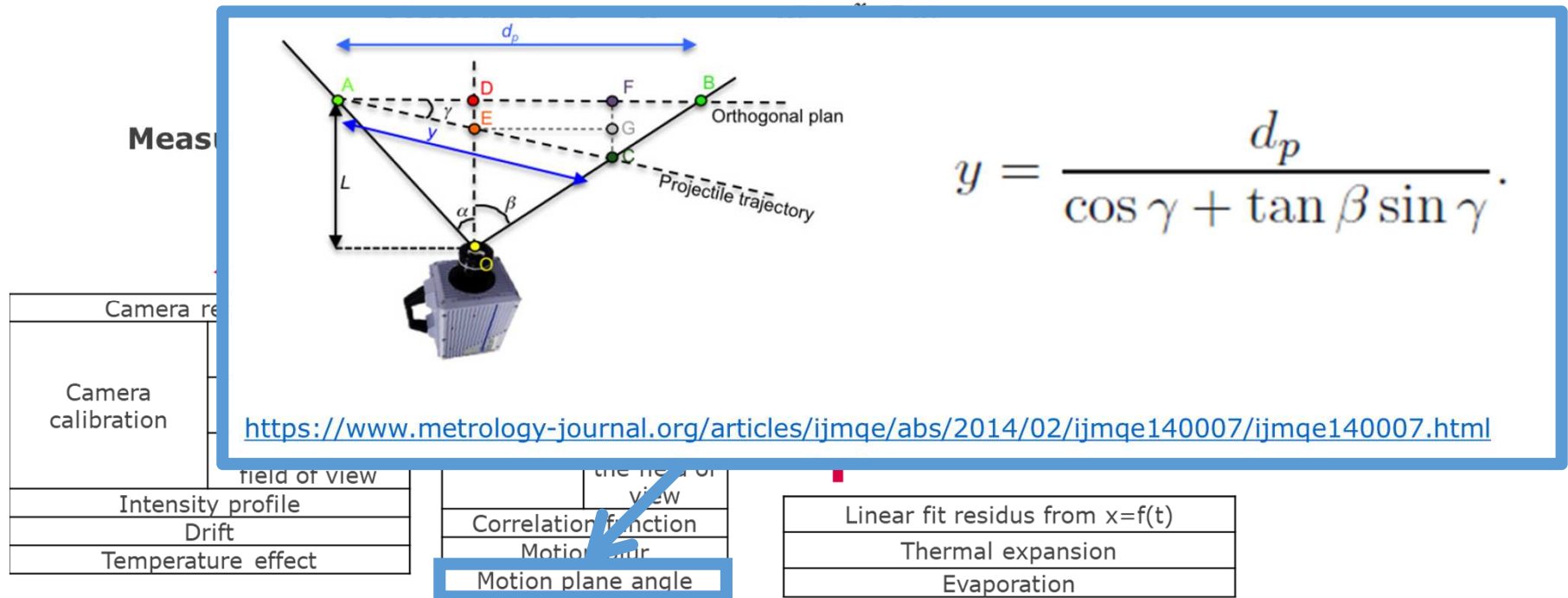


For 5 nl/min :

$U(Q_{ref}) = 11 \% (k=2)$ for a 1 second measurement at 5 fps

$U(Q_{ref}) = 0.5 \% (k=2)$ for a 120 seconds measurement at 5 fps

Interface Tracking: principle at CETIAT Uncertainty Budget



For 5 nl/min :

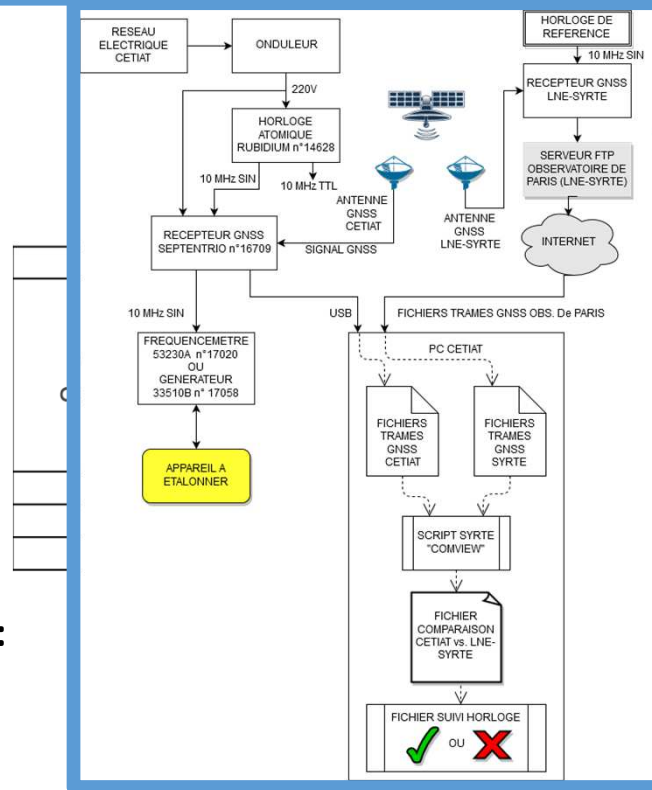
$U(Q_{ref}) = 11 \% (k=2)$ for a 1 second measurement at 5 fps

$U(Q_{ref}) = 0.5 \% (k=2)$ for a 120 seconds measurement at 5 fps

Interface Tracking: principle at CETIAT Uncertainty Budget

$$R^2 = \frac{x}{t} \cdot \frac{\pi}{4} R^2$$

CETIAT's Time & Frequency Traceability Chain



$$u(Q_V) = \sqrt{\left(\frac{\partial Q_V}{\partial d}\right)^2 \cdot u^2(d) + \left(\frac{\partial Q_V}{\partial x}\right)^2 \cdot u^2(x) + \left(\frac{\partial Q_V}{\partial t}\right)^2 \cdot u^2(t)}$$

displacement

time

Calibration of the signal generator
Exposure time
Drift
Temperature effect

+

Linear fit residus from x=f(t)
Thermal expansion
Evaporation

- Resolution
- Objective micrometer
- Position in the focal plane
- Position in the field of view
- Position function
- Position blur
- Plane angle

For 5 nl/min :

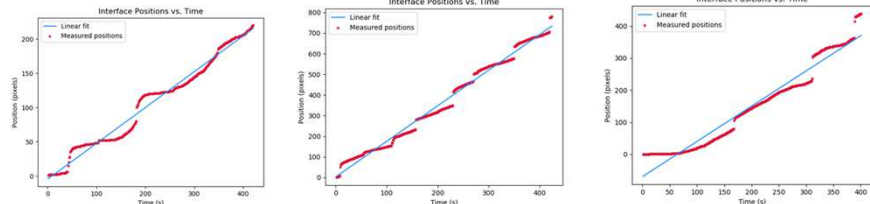
for a 1 second measurement at 5 fps
for a 120 seconds measurement at 5 fps

Interface Tracking: principle at CETIAT

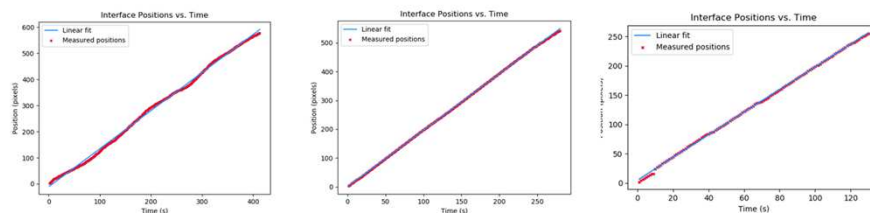
Uncertainty Budget

Slip & Stick Effect

Uncoated capillary

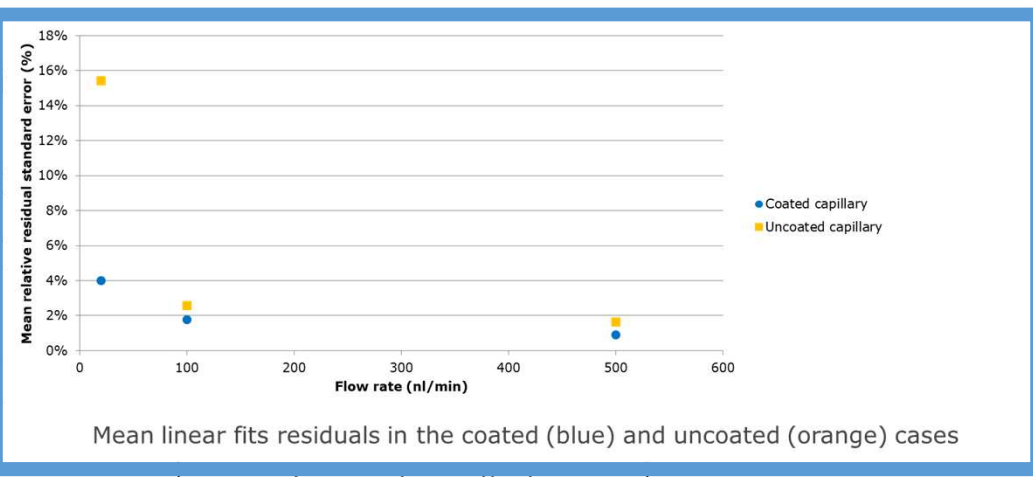


Coated capillary



temperature effect

Motion plane angle



Mean linear fits residuals in the coated (blue) and uncoated (orange) cases

temperature effect

Linear fit residus from $x=f(t)$

Thermal expansion

Evaporation

For 5 nl/min :

$U(Q_{ref}) = 11 \% (k=2)$ for a 1 second measurement at 5 fps

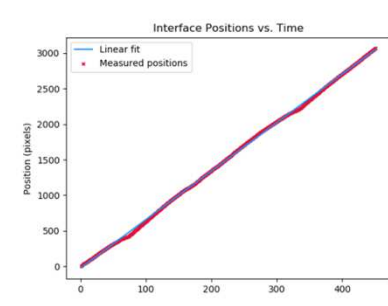
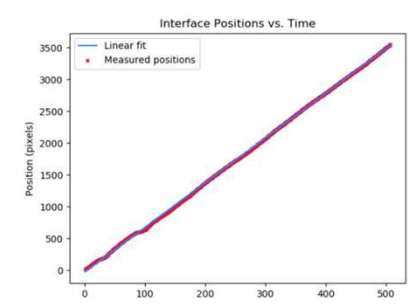
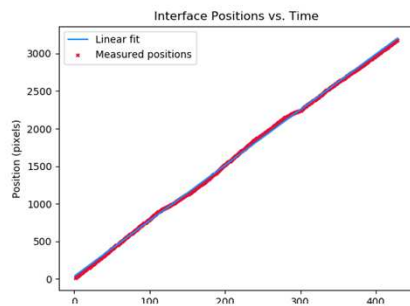
$U(Q_{ref}) = 0.5 \% (k=2)$ for a 120 seconds measurement at 5 fps

Interface Tracking: principle at CETIAT

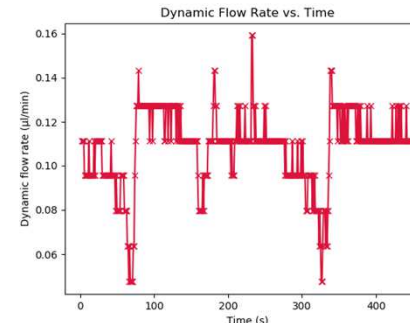
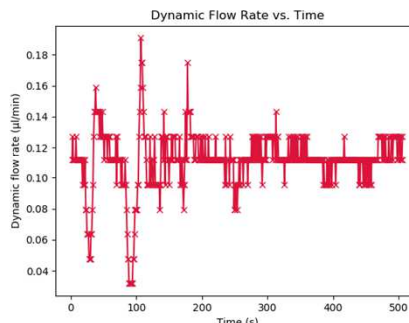
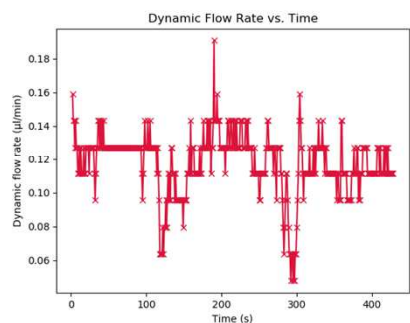
Dynamic flows

Generated flow rate
= 100 nl/min

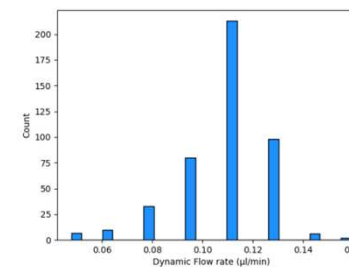
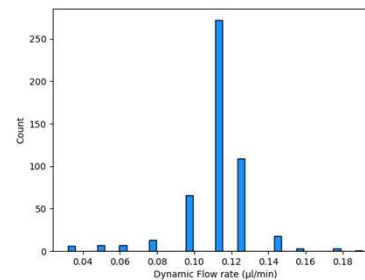
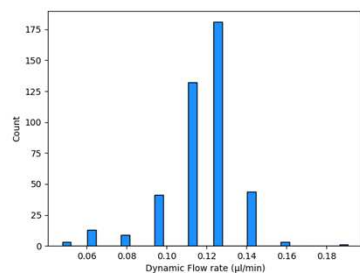
Determination of the mean
flow rate



Dynamic flow rate
(1 point/s)

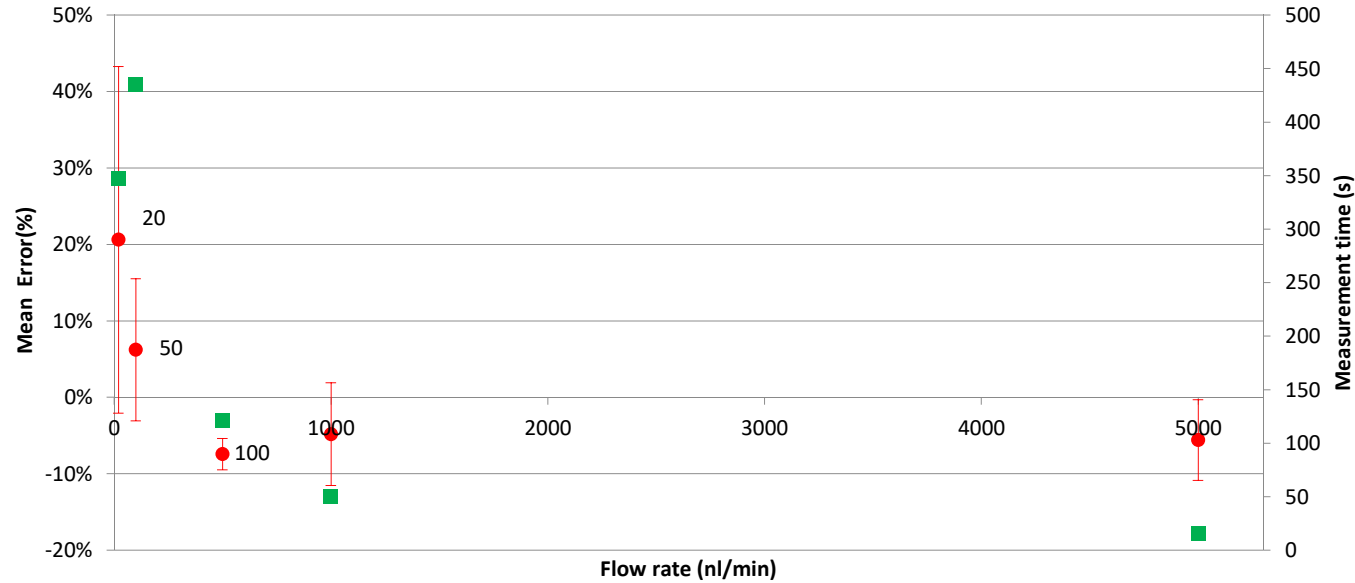


Dynamic flow rates
distribution



Interface Tracking: calibration example At CETIAT

Calibration Results of a Coriolis flow meter

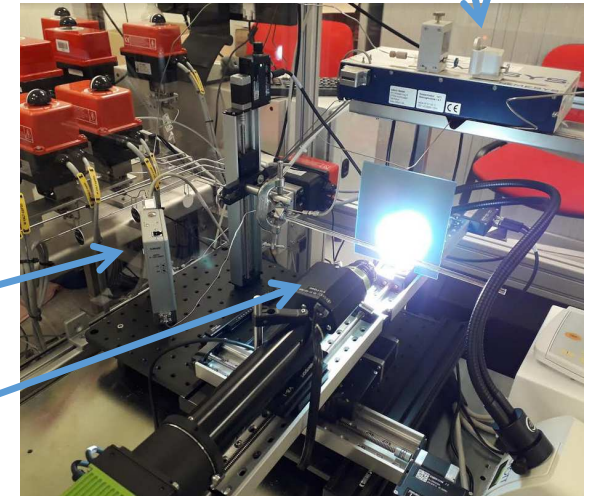


Flow generator
(syringe pump)

● Mean Error (%)
■ measurement time (s)

Flow meter under test

Front tracking system
(reference flow rate)





Interface Tracking setup at IPQ (Portugal)

EMPIR

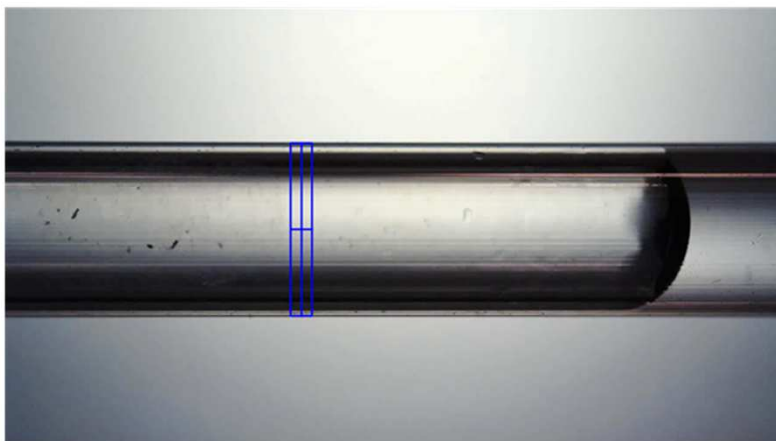
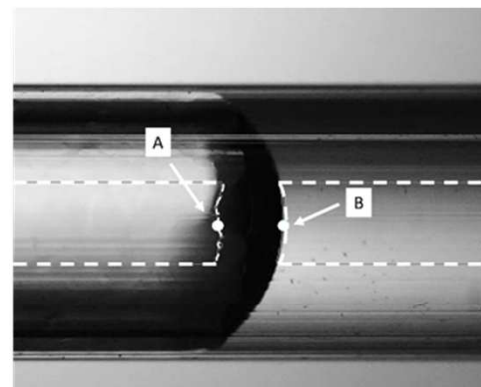


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Interface Tracking at IPQ

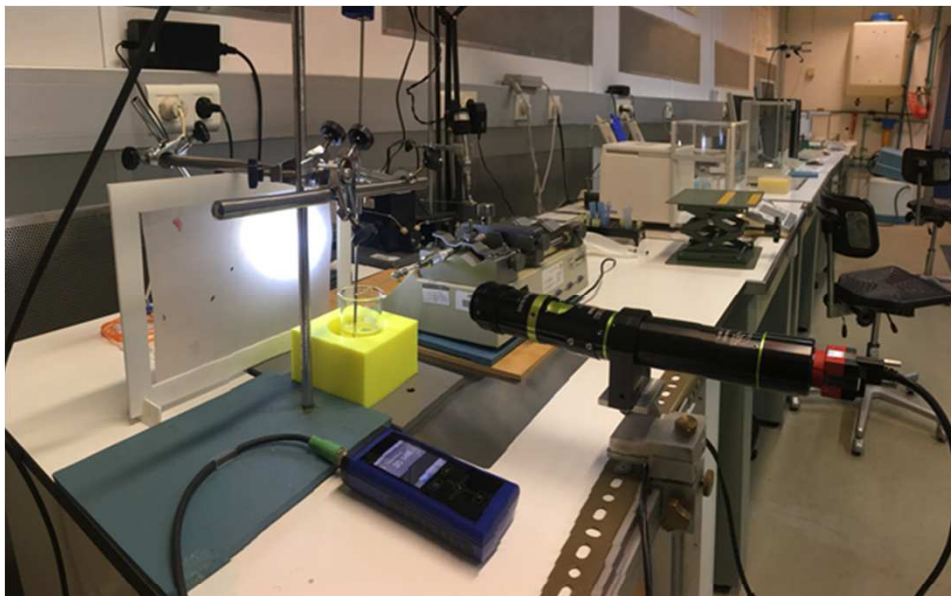


The experimental setup consists of using a high-resolution camera and an Python image processing software to track the distance traveled by the meniscus of a liquid in a capillary tube and calculate the flow rate.



To determine the position of the meniscus over time it was assumed as reference the position of the point that is in the axis of the capillary and coincident with the meniscus.

Interface Tracking at IPQ



$$Q = \frac{x_2 - x_1}{\Delta t} \times \pi \times r^2 \times [1 - \gamma (T - 20)]$$

Can go down 1 $\mu\text{L/h}$ with 7 % uncertainty



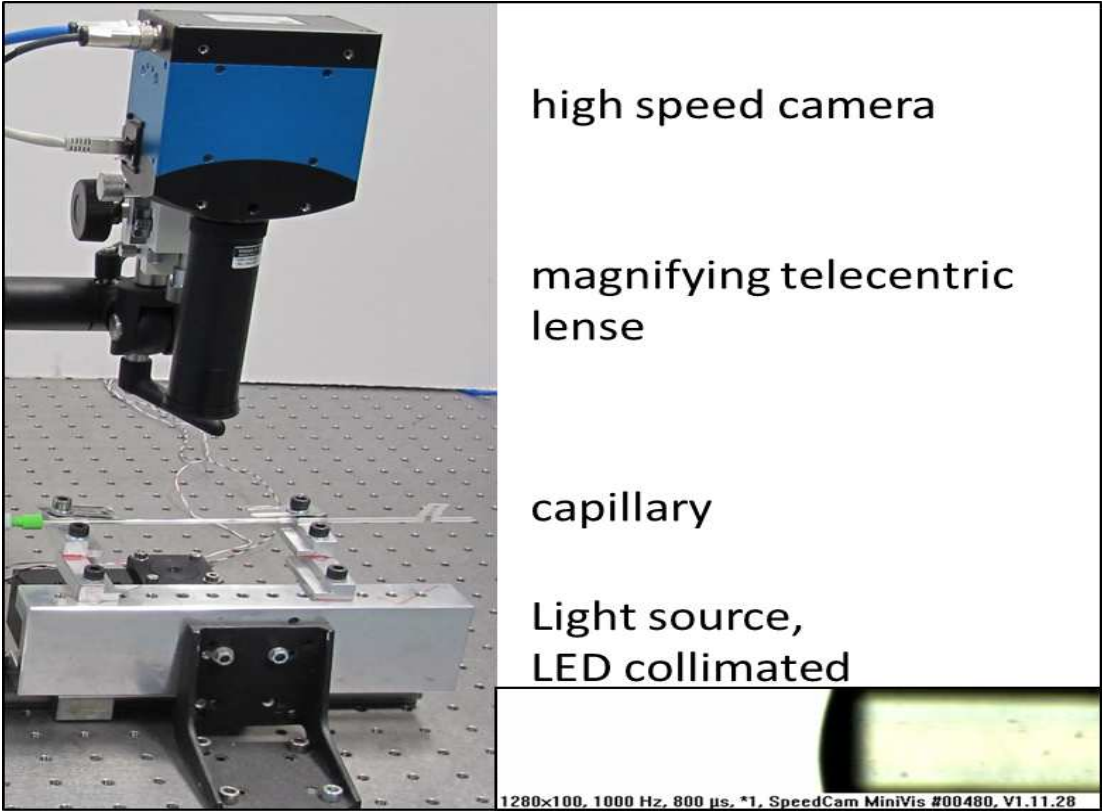
Interface Tracking setup at THL (Germany)

EMPIR



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Interface Tracking at THL



high speed camera

magnifying telecentric
lense

capillary

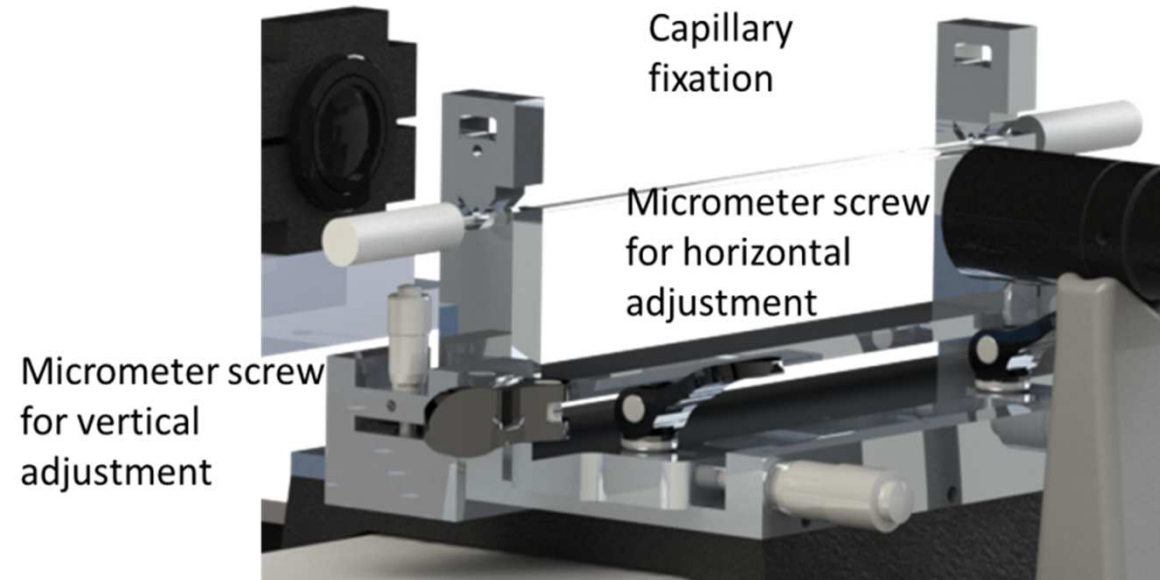
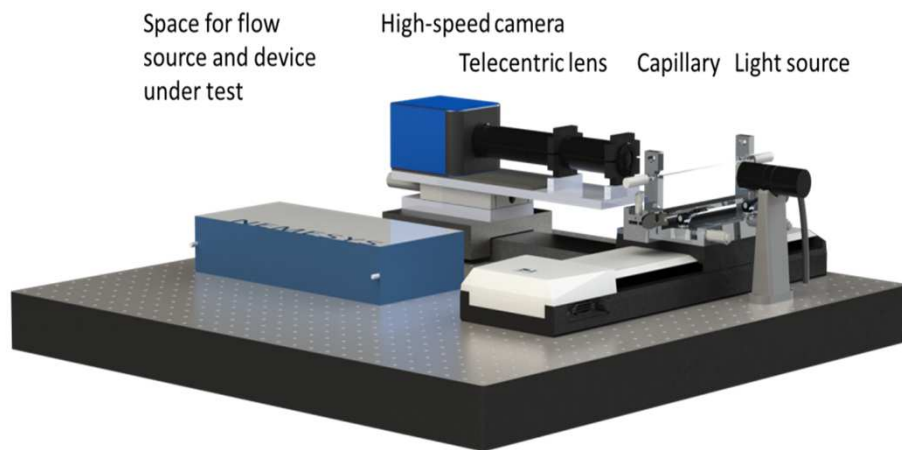
Light source,
LED collimated

1280x100, 1000 Hz, 800 μs, *1, SpeedCam MiniVis #00480, V1.11.28



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Interface Tracking at THL



facility used between 50 nl/min and 500 μ l/min.

Interface Tracking at THL

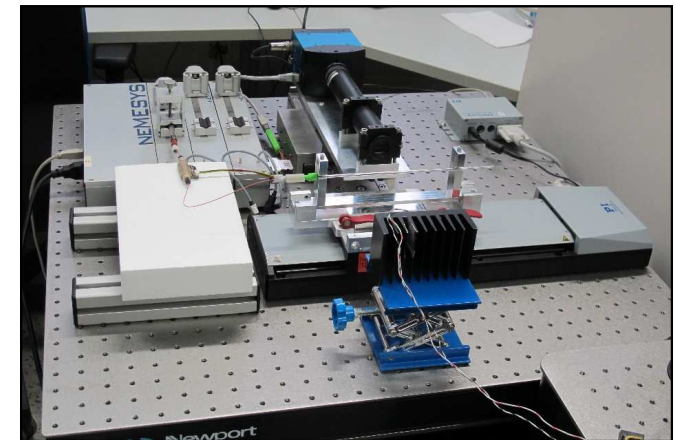
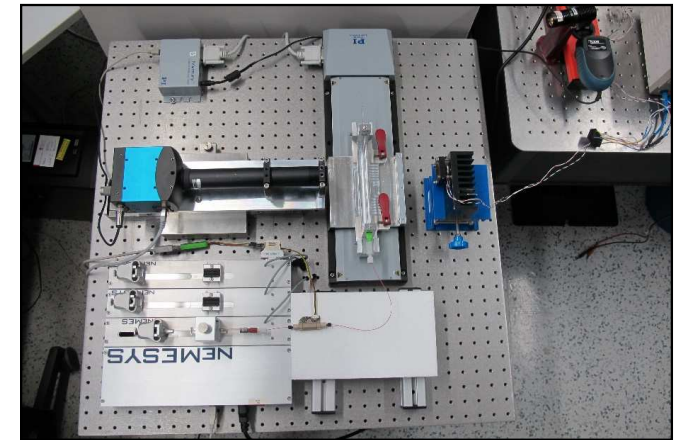
Components

1. Optical table
2. High speed camera
3. Light source
4. Precision Linear Stage
5. Device under examination

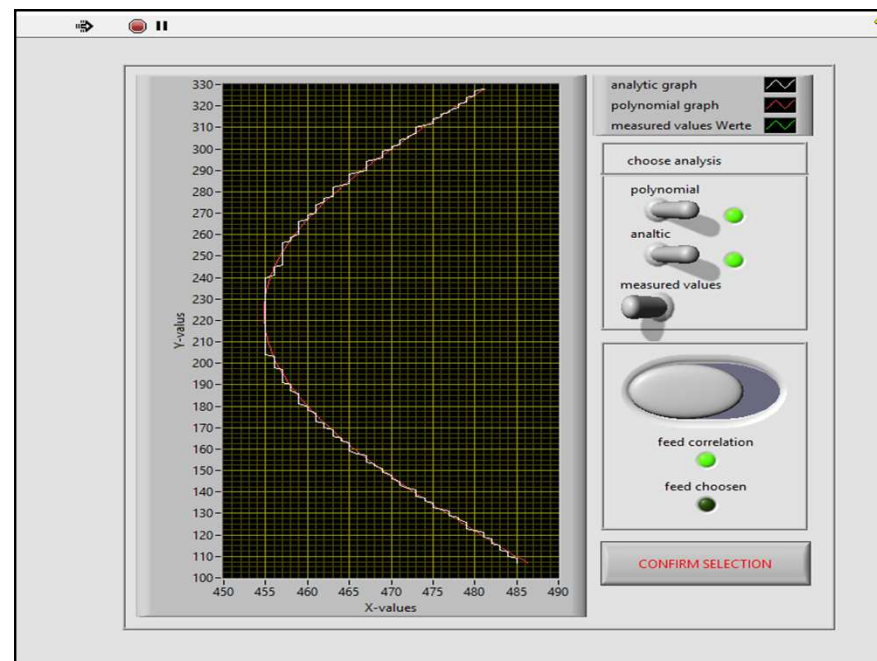
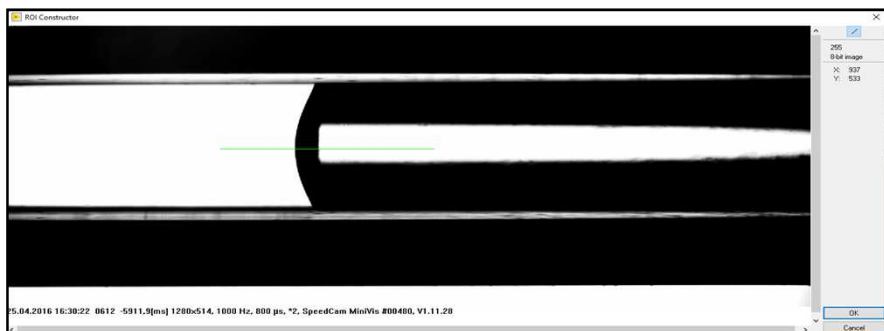
Flow dosing unit

Flow sensor

Capillaries

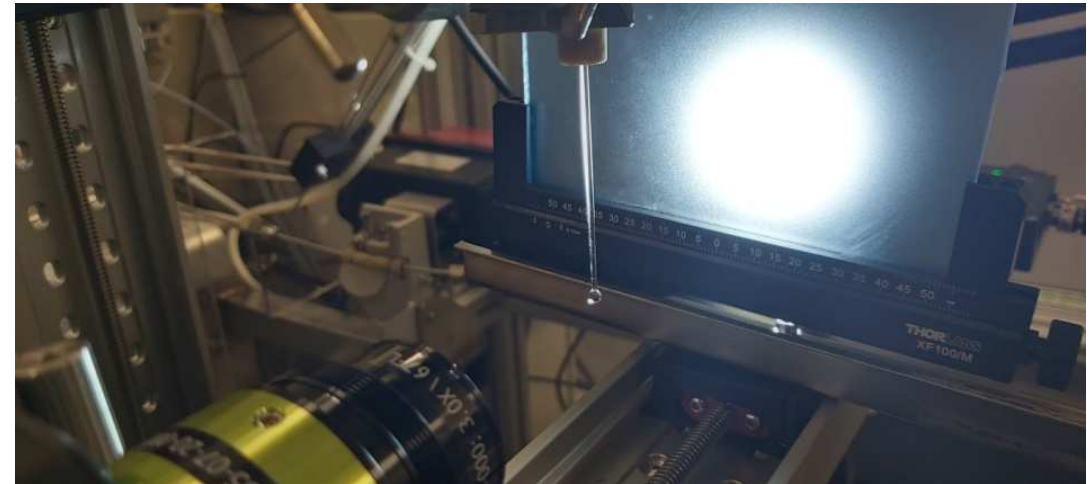
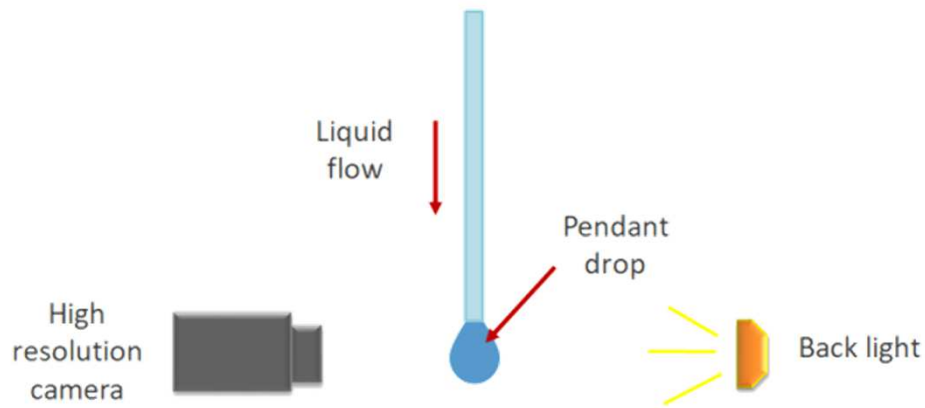


Interface Tracking at THL



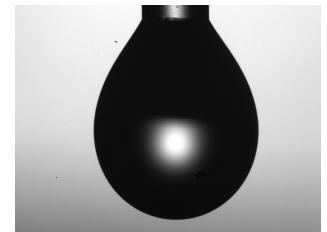
Pendant Drop Method at CETIAT (France)

Pendant Drop method at CETIAT

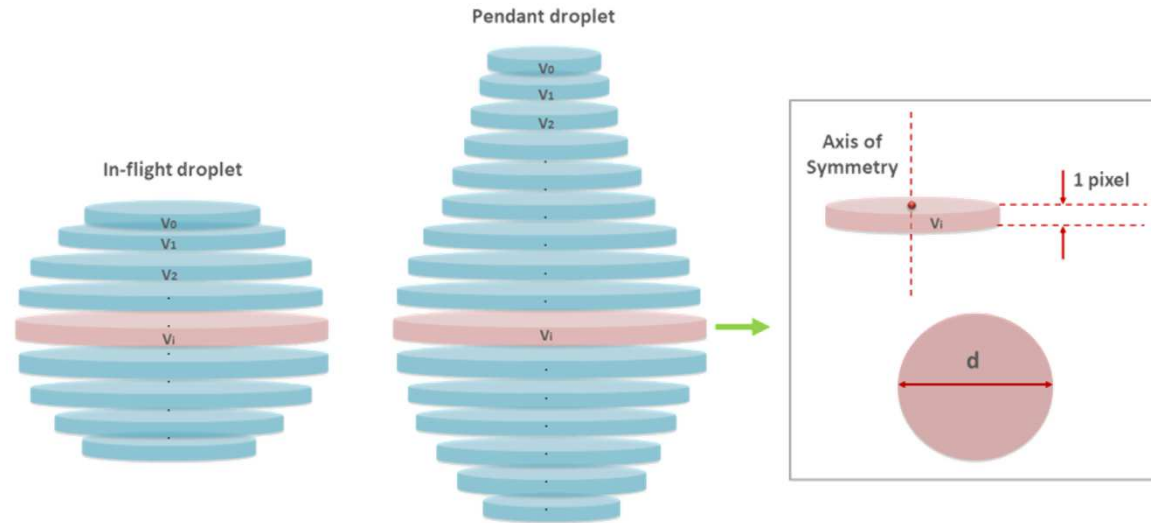


Measurement of the change in the droplet's volume over time under a liquid flow

$$Q_V = \frac{\Delta V_{droplet}}{\Delta t}$$

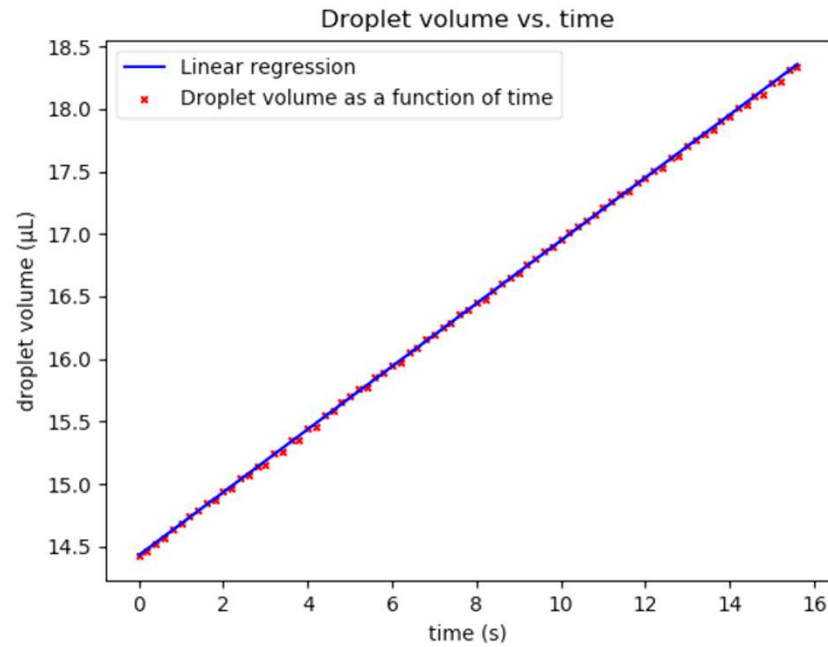


Pendant Drop method at CETIAT

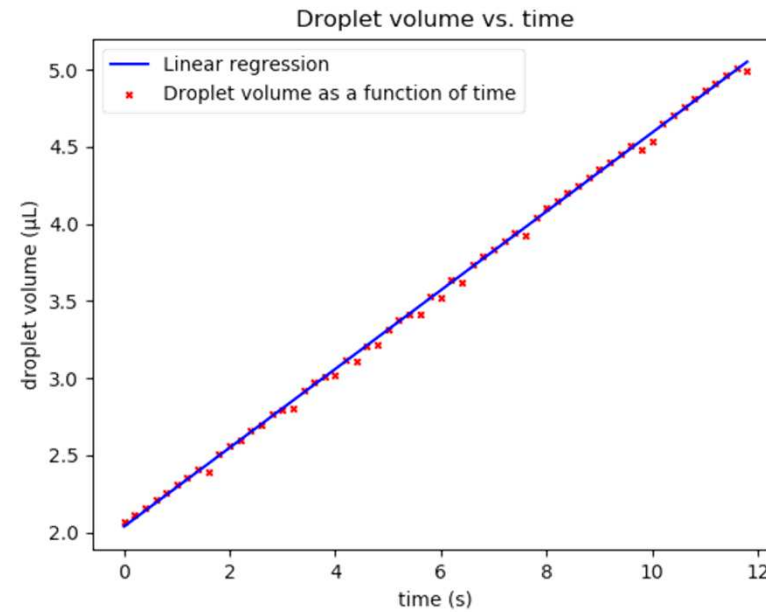


$$V_{droplet} = \sum_{i=1} V_i = \sum_{i=1} \frac{\pi}{4} d_i^2 \cdot h \quad \longrightarrow \quad Q_V = \frac{\Delta V_{droplet}}{\Delta t}$$

Pendant Drop method at CETIAT



Q = 15,10 µl/min

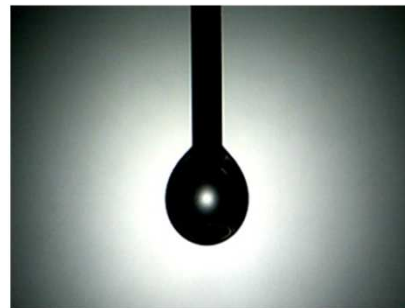
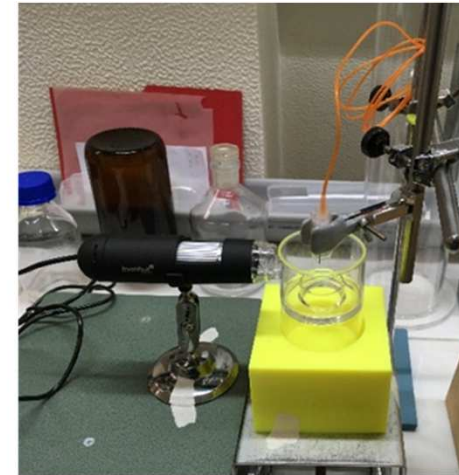


Q = 15,31 µl/min

Pendant Drop Method at IPQ (Portugal)

Pendant Drop method at IPQ

The delivered liquid flow was determined by observing the volume increase of a drop at the end of the flow line placed inside an evaporation trap.



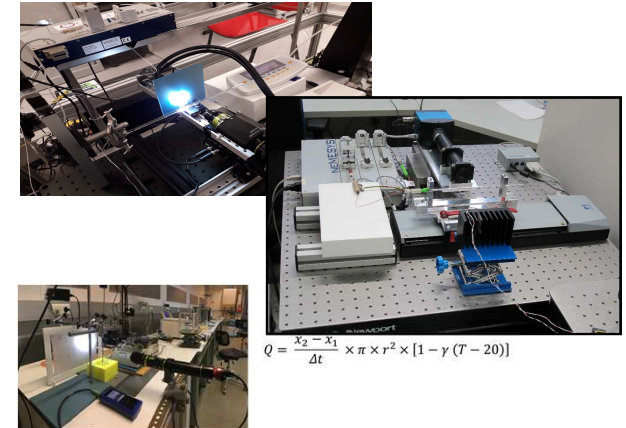
This observation was performed at a specific time by using photographs taken by a digital USB microscope with 400X magnification and a Phyton software for image treatment.

$$Q = \frac{\Delta V}{\Delta t}$$

CONCLUSION

1. Interface tracking method

- Principle (example at CETIAT)
- Uncertainty budget (example at CETIAT)
- IPQ & THL Interface Tracking Setups

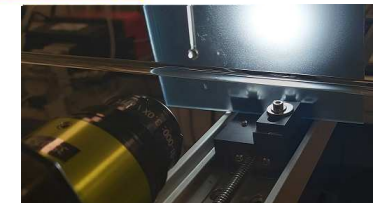


$$Q = \frac{x_2 - x_1}{\Delta t} \times \pi \times r^2 \times [1 - \gamma (T - 20)]$$

2. Pendant drop method

- Principle (example at CETIAT)
- IPQ Pendant Drop setup

Can go down 1 $\mu\text{L/h}$ with 7 % uncertainty



The delivered liquid flow was determined by observing the volume increase of a drop at the end of the flow line placed inside an evaporation trap.



This observation was performed at a specific time by using photographs taken by a digital USB microscope with 400X magnification and a Python software for image treatment.

$$Q = \frac{\Delta V}{\Delta t}$$